<u>IN THE SPECIFICATION</u>:

Please amend the Specification as follows:

Please amend the paragraph on page 17, lines 10-14 as follows:

The roots of the trunnion barrel and the trunnion journal may be of two-step shape, and the corner at the trunnion journal may be ~~one R surface, or~~ a ~~round surface, continuously extending with~~ <u>continuous surface having</u> a predetermined radius of curvature.

Please amend the paragraph bridging pages 23-24 of the originally filed Specification as follows:

The relief portions 15a and 15b, as seen in a cross section (Fig. 1), are each, respectively, formed by an arcuate curve smoothly connected to a corresponding end of the roller guide surface 14 to the minor and major inner diameter portions 16 and 18 of the outer joint member 10. As shown in Fig. 1A, the relief portions 15a and 15b (only relief portion 15b is shown for exemplary purposes) ~~is~~ <u>are</u> connected to the radius of curvature R of the roller guide surface 14 at a corner K. In the embodiment shown by way of example in Fig. 1, the length of the contact ellipse shown in two-dot chain lines is equal to the distance between the points of connection between the roller guide surfaces 14 and the relief portion 15a and 15b.

Please amend the paragraph bridging pages 28-29 of the Specification as follows:

The first, second, and third embodiments are the same as far as the basic construction of tripod joint is concerned and as previously described in connection with Figs. 2A, 2B, 3A, 3B, and 3C. Here, the root of the trunnion journal 22, as shown in Fig.

8A, is of two-step shape. That is, a step portion rising from the trunnion barrel 21 is formed and a cylindrical outer peripheral surface 24 extends from the step portion. The corner at the base end of the cylindrical outer peripheral surface 24 is one continuous [[R]] surface having a predetermined radius of curvature Rb. In the case of prior art shown in Fig. 8B, the trunnion barrel 21' directly connects to the cylindrical outer peripheral surface 24' through ~~an R~~ <u>a</u> surface having a radius of curvature Ra. As is apparent from a comparison between the two figures, there are relations Ra > Rb and tw1 > tw2.

Please amend the paragraphs on page 30, line 1 to page 32, line 5 of the Specification as follows:

~~The proportion 100~~ <u>A ratio or proportion</u> (φds/PCD) of shaft diameter/PCD was set to 50% - 55%. The shaft diameter φds was determined from the allowable load capacity, and the pitch circle diameter PCD of the roller guide surface 14 was determined from the ratio of the width Ls of the roller 30 to the outer diameter φDs.

~~The proportion 100~~ <u>A ratio or proportion</u> (φdr/SDj) of trunnion barrel diameter / outer diameter of the trunnion was set to 65% -70%. The trunnion barrel diameter φdr was determined from the torsional strength during the application of a predetermined torque, and the trunnion outer diameter SDj was determined from the width Ls of the roller 30, the washer height, and the major inner diameter φD1 of the outer joint member 10.

~~The proportion 100~~ <u>A ratio or proportion</u> (φD2/φD1) of minor inner diameter / major inner diameter of the outer joint member 10 was set to 66 – 72%. The minor inner diameter φD2 of the outer joint member 10 was set to a value which allows the

securing of an operating region for the shaft diameter φds and trunnion barrel diameter φdr, and the major inner diameter D1 was determined from the pitch circle diameter PCD of the track groove 12 and the trunnion outer diameter SDj.

~~The proportion 100~~ A ratio or proportion (Ls/φDs) of width/outer diameter of the roller 30 was set to 24% - 27%. The width Ls and outer diameter φDs of the roller 30 were set to optimum values by considering the contact ellipse length and contact surface pressure between the roller 30 and the roller guide surface 14 when a predetermined ~~toque~~ torque was applied.

~~The proportion 100~~ A ratio or proportion (φDj/φDs) of trunnion journal diameter/roller outer diameter was set to 54% - 57%. The trunnion journal diameter φDj was made equal to the current dimension in order to secure torsional strength, and the roller outer diameter φDs was set on the basis of the contact surface pressure.

~~The proportion 100~~ A ratio or proportion (φDj/φds) of trunnion journal diameter/shaft diameter was set to 83% - 86%. It was set to the same dimension as the current proportion in order to secure torsional strength and durability.

~~The proportion 100~~ A ratio or proportion (Ln/φDj) of needle roller length/trunnion journal diameter was set to 47% - 50%. The needle roller length Ln was set by considering the maximum contact surface pressure for the bearing. In addition, by reducing the size of the root [[R]] of the trunnion journal 22 and thinning the inner washer to correspondingly increase the diameter of the root to provide a stepped shape, the wall thickness between the root and the serrations increases and it is also possible to increase the torsional strength.